

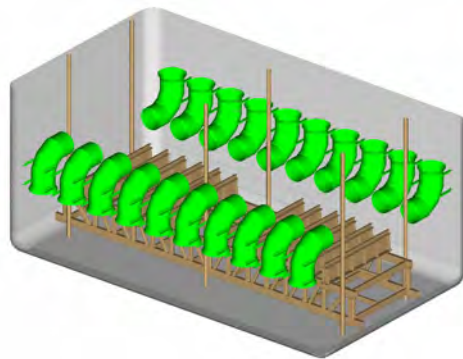
Development of Quench Tank Agitation Design Using CFD Modeling

John D. Nitz, PE
Project Engineer

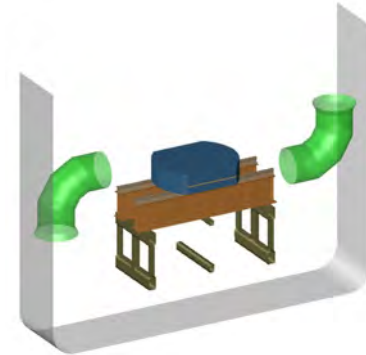
Airflow Sciences
Corporation



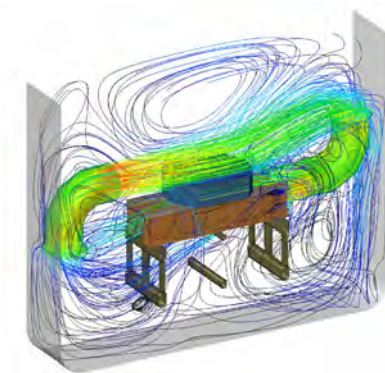
Iterative Design Process - Overview



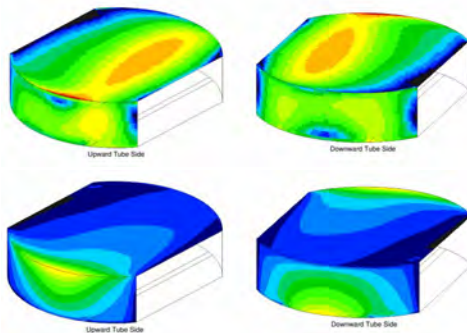
System Design
(CAD Geometry)



CFD Model
(Symmetry Section)



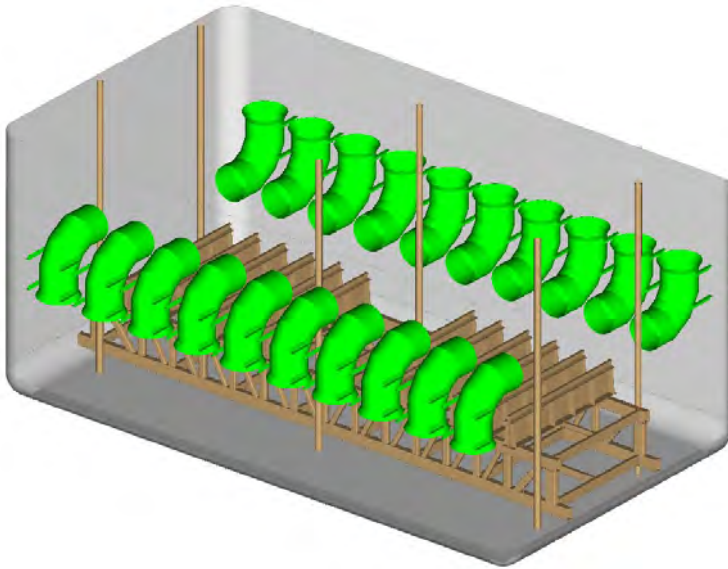
Predicted Flow Field



Calculated Velocity Profile & Heat Transfer Coefficients
(Surrogate Part)



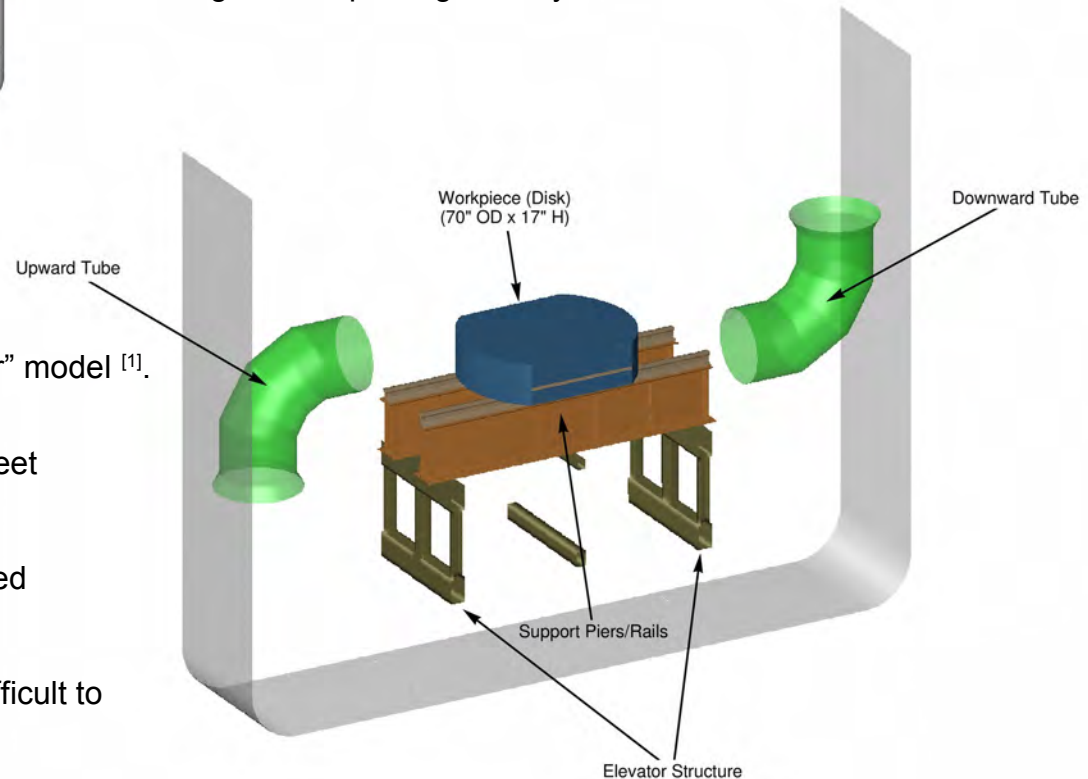
Baseline Design – CFD Model Geometry



Baseline CAD Design

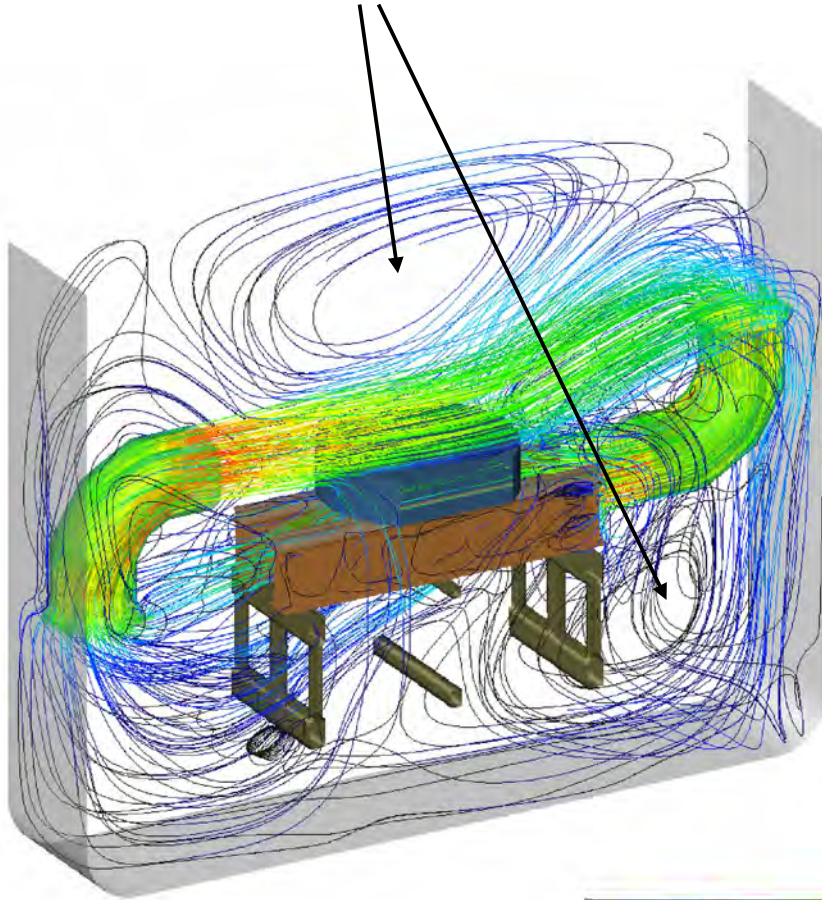
- Discrete, opposing draft tube concept (upward / downward).
- Variable vertical working envelope.
- Forced circulation across width of tank (minimal lengthwise flow).
- CFD model represents symmetry section (one tube pair).
- Surrogate workpiece geometry for evaluation.

- Impellers simulated using computational “propeller” model ^[1].
- Fluid momentum and pressure rise specified to meet target flow rate (21,500 GPM).
- Rotational component specified based on estimated impeller efficiency.
- Actual impeller geometry is preferred, but more difficult to obtain.

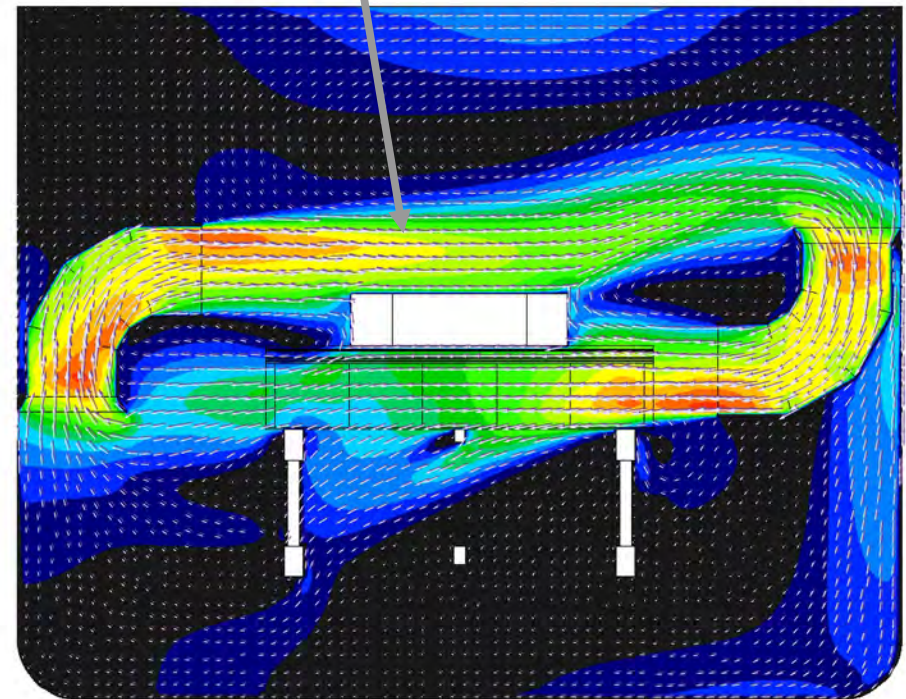


Baseline Design – CFD Results

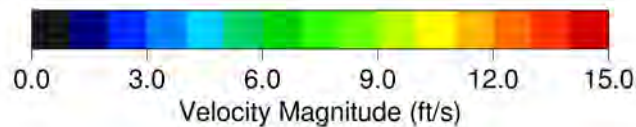
Low velocity re-circulation zones above and below workpiece



High velocity jets vertically localized in work zone.

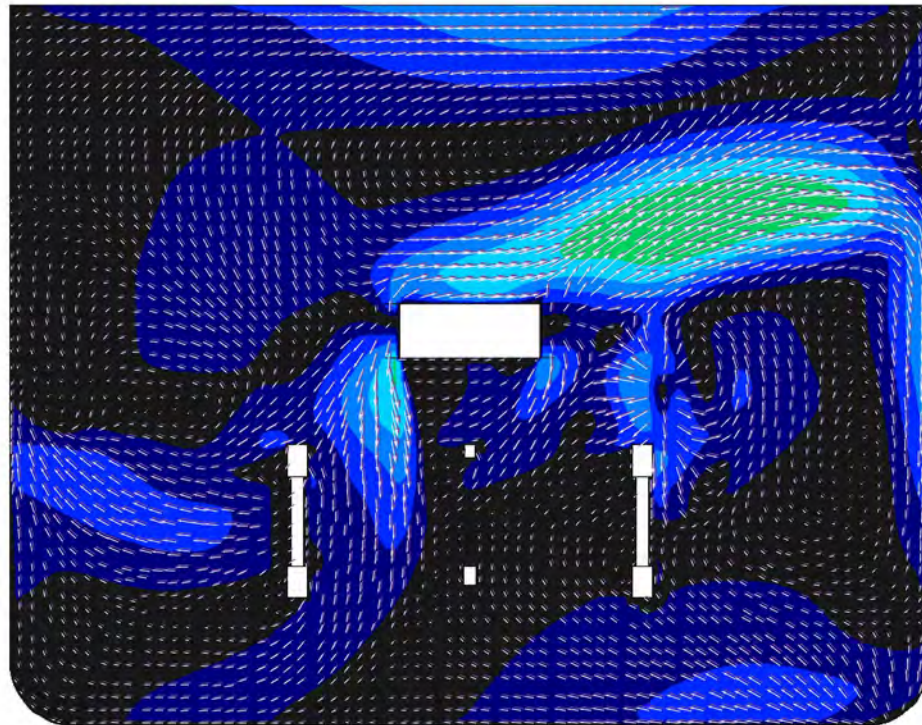
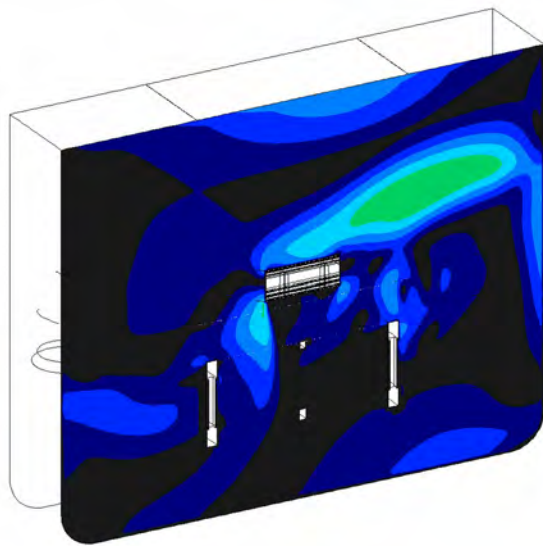


Impeller Center Line Plane

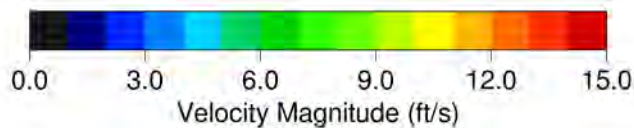


Baseline Design – CFD Results

Low velocities between impellers / draft tubes.

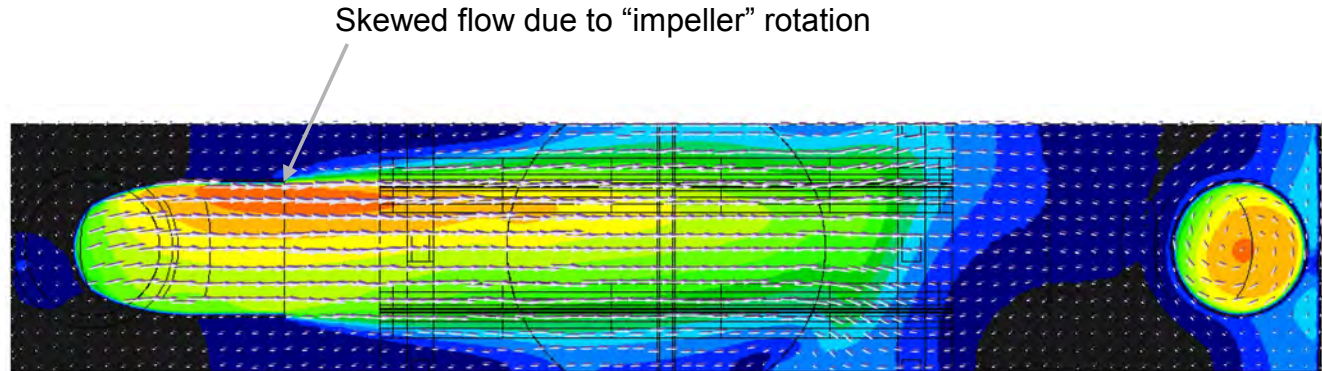
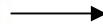
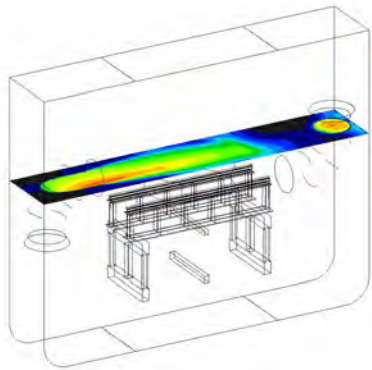


Plane Between Impellers



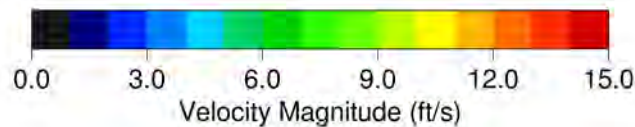
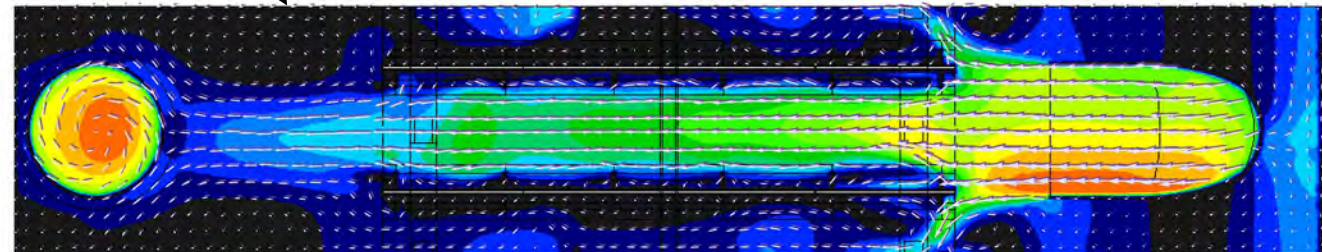
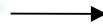
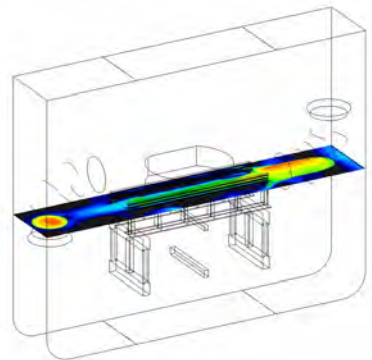
Baseline Design – CFD Results

Horizontal section cuts



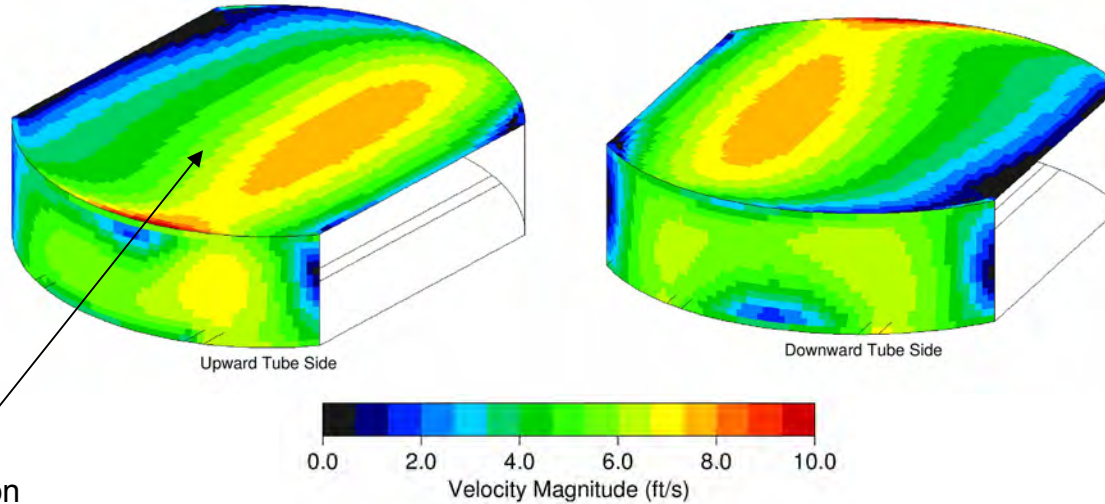
Localized flow above workpiece

Low velocities between draft tubes



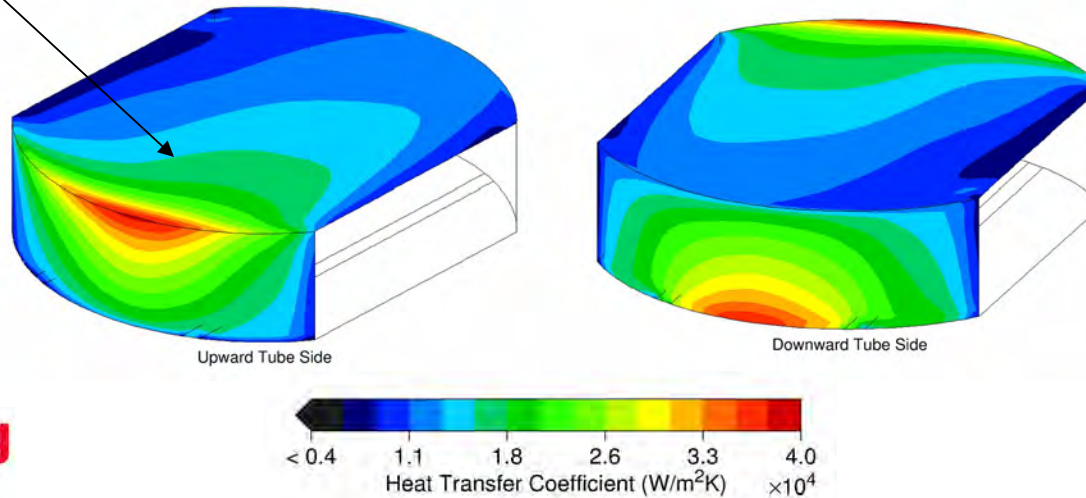
Baseline Design – CFD Results

Near-surface velocity

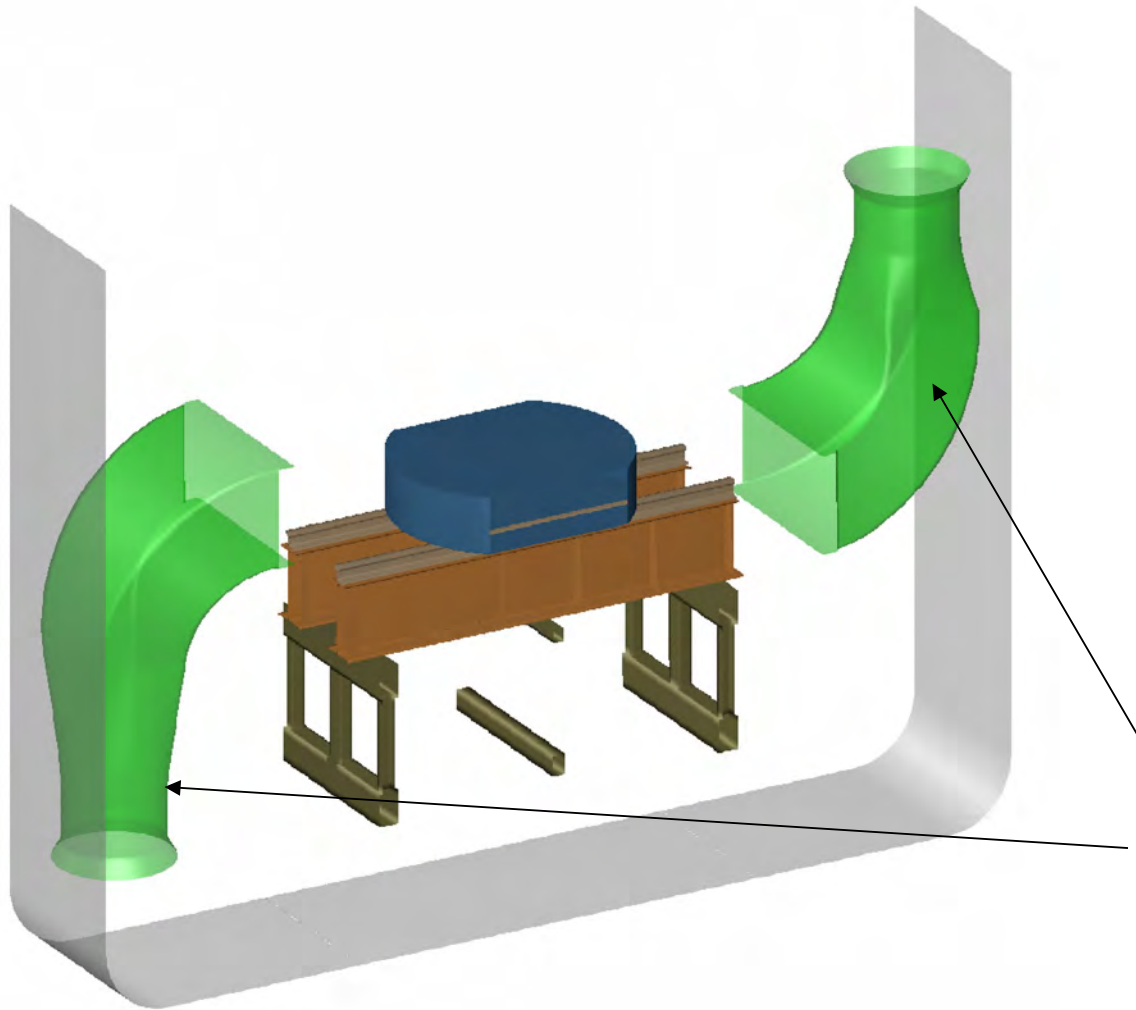


Skewed distribution
due to impeller rotation

Surface heat transfer coefficient

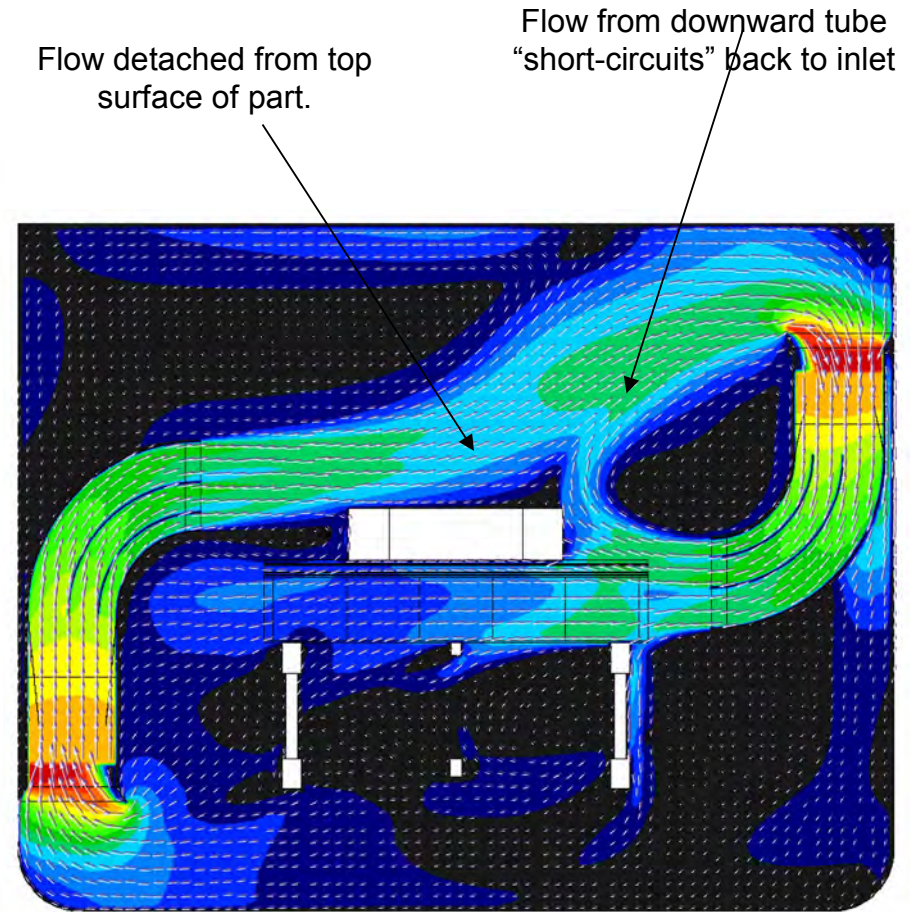
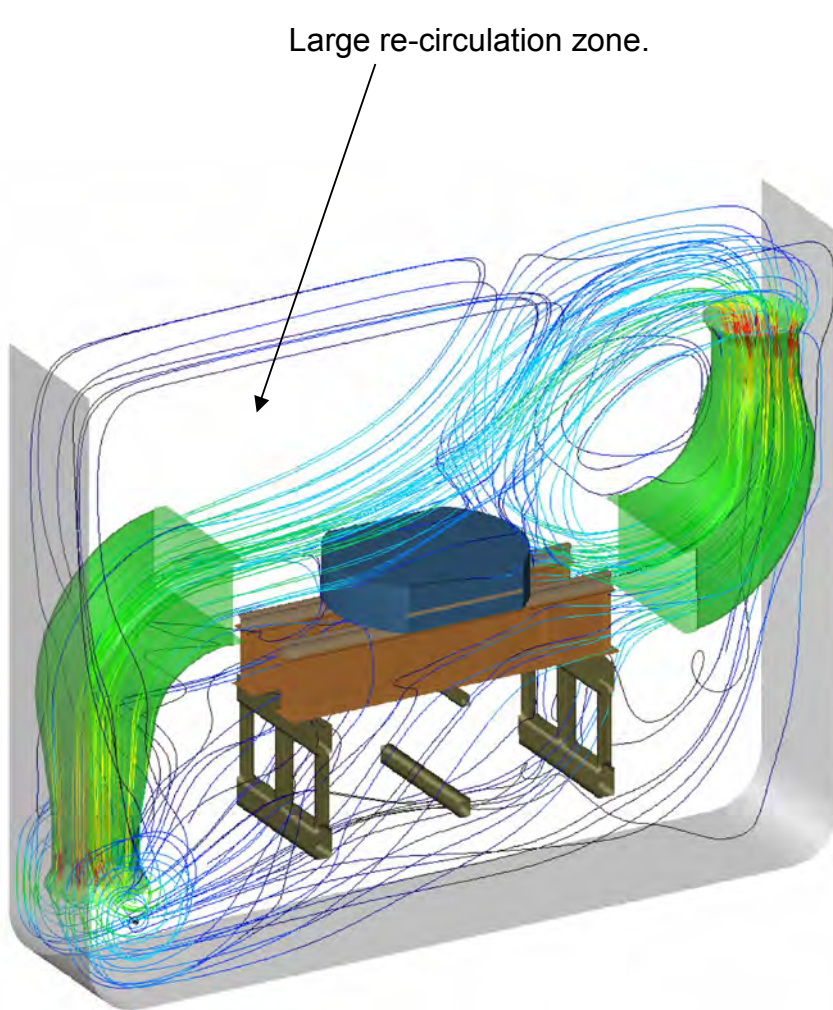


Intermediate Design – CFD Model Geometry

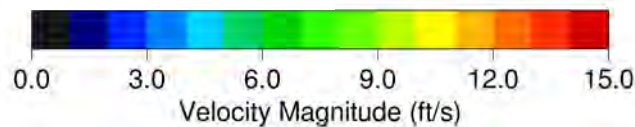


- Transition to rectangular outlets.
- Taller intake tubes.
- Internal turning vanes (not shown).

Intermediate Design – CFD Model Geometry

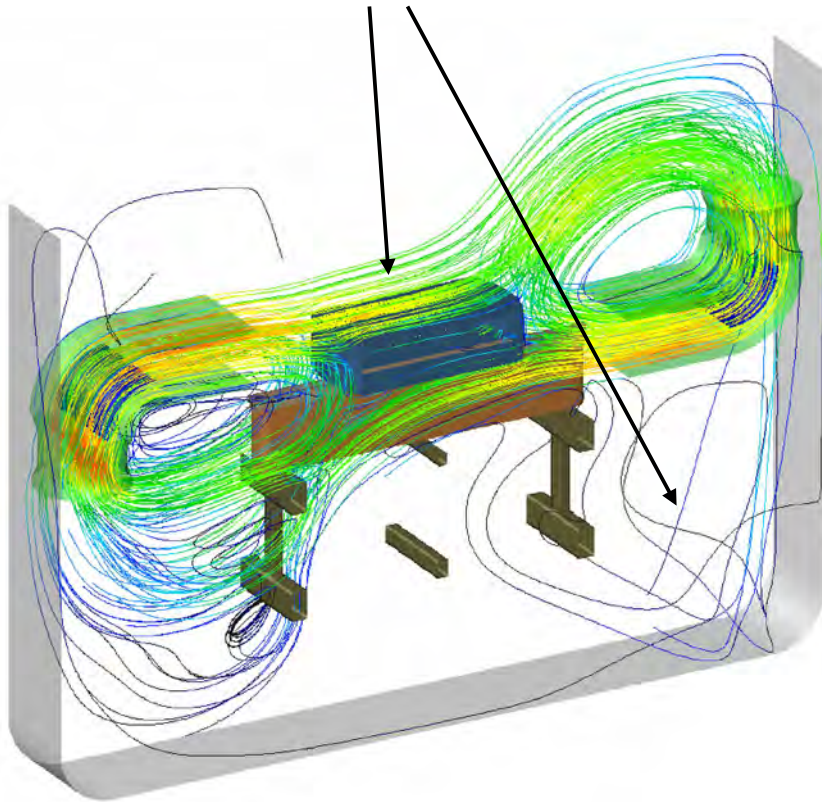


Impeller Center Line Plane

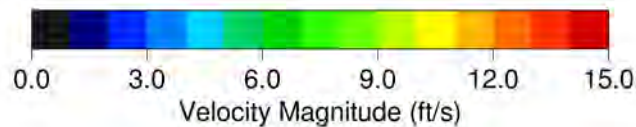
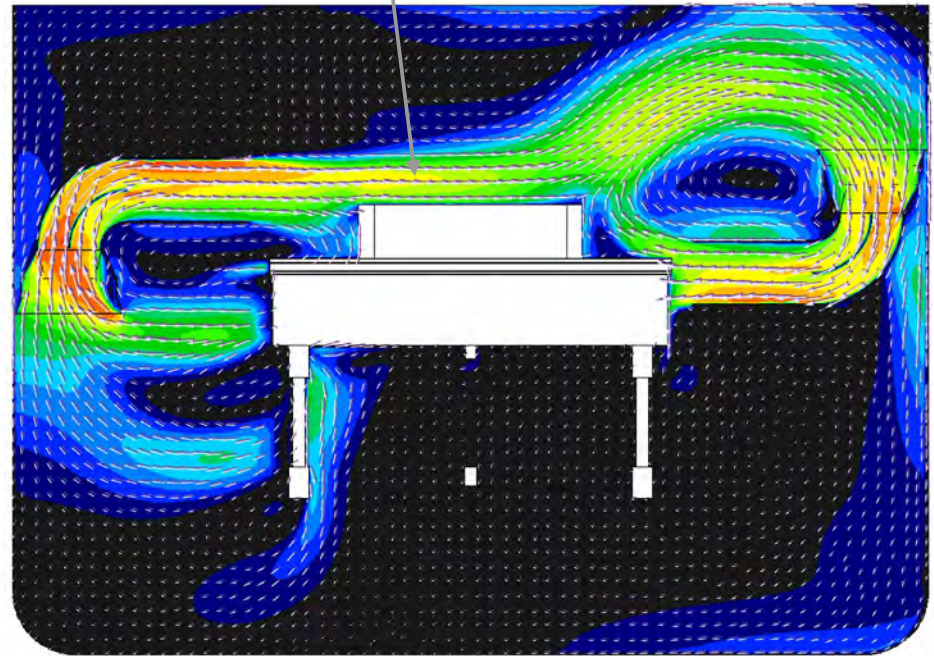


Final Design – CFD Results

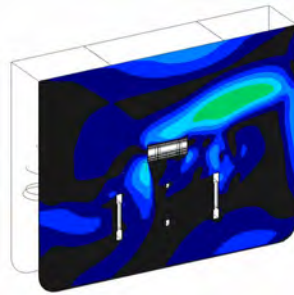
Stronger flow through work-zone.
Reduced re-circulation at top and bottom of tank.



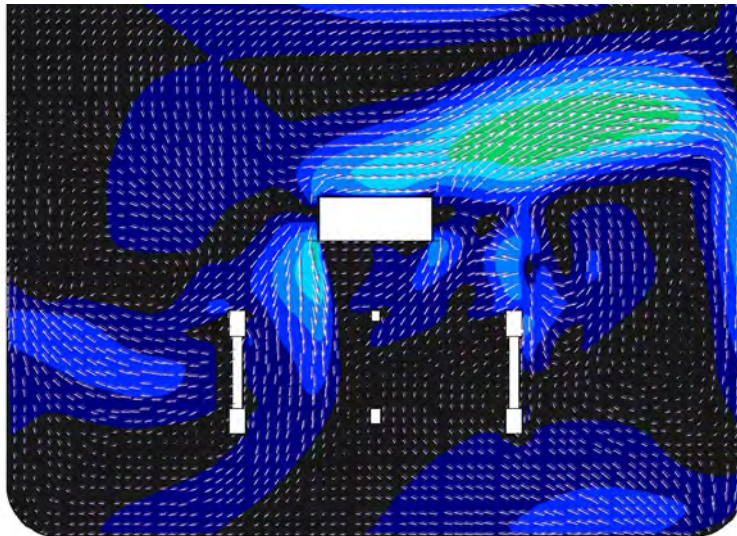
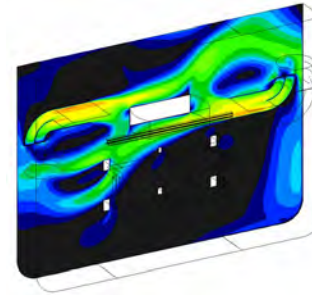
Fluid jets localized near
part surface.



Final Design – CFD Results

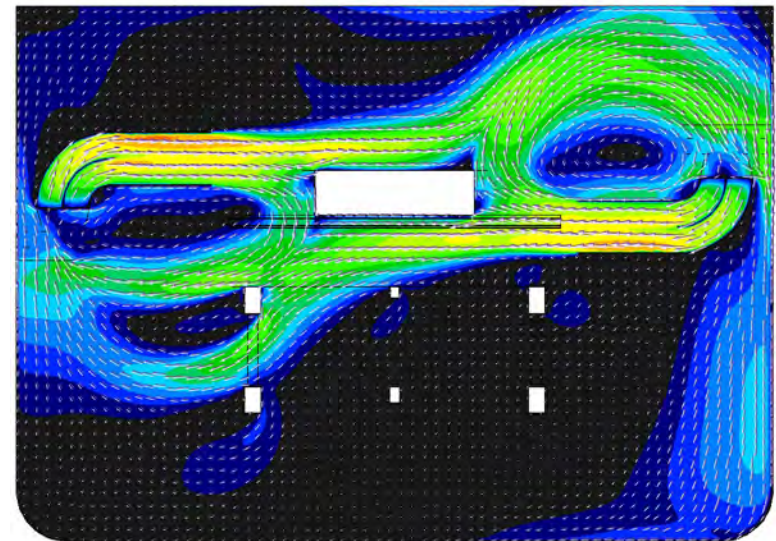


Planes Between Impellers



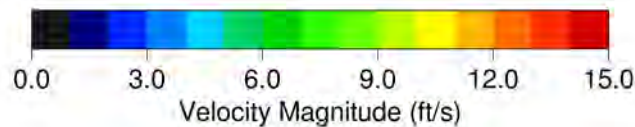
Original Design

Low velocities between impeller tubes.



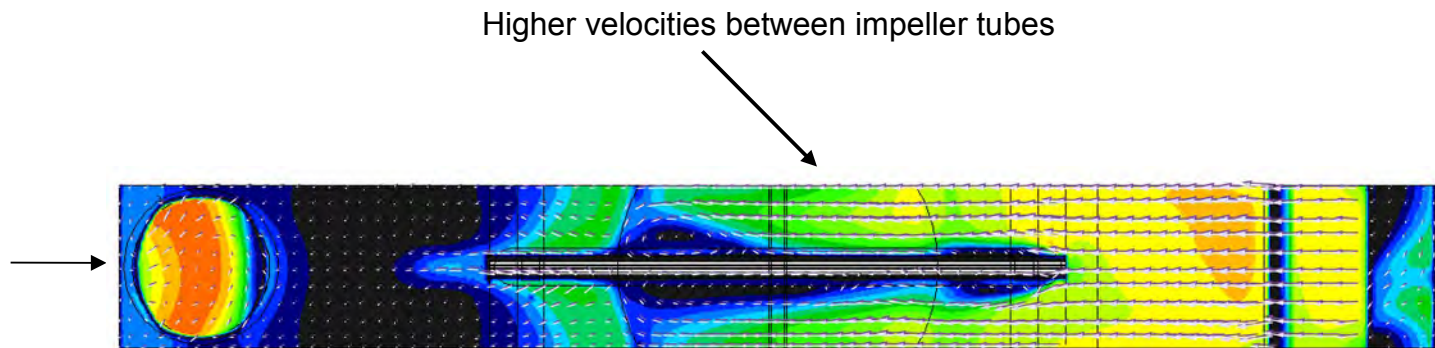
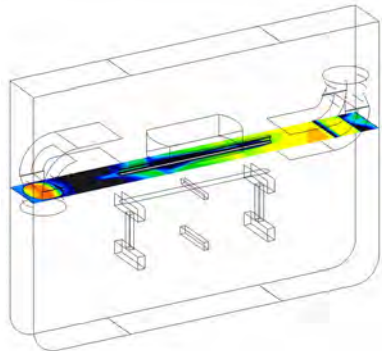
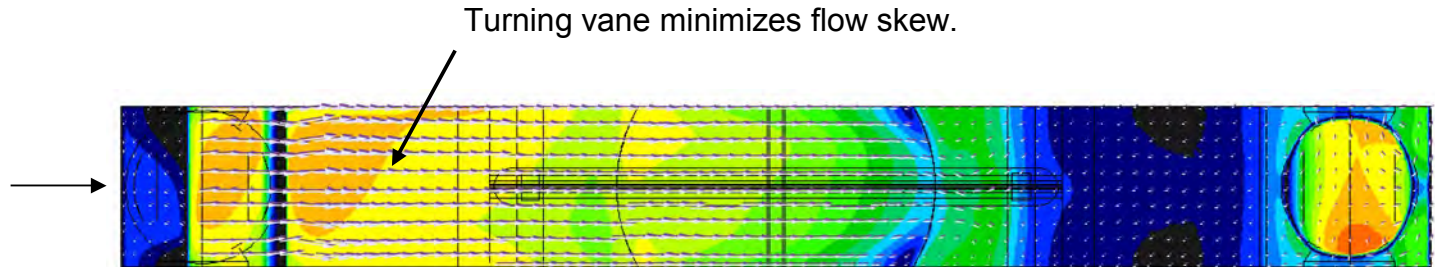
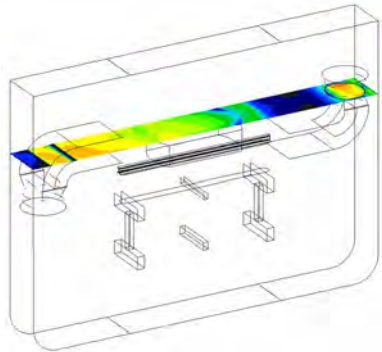
Final Design

Improved velocities between impeller tubes.

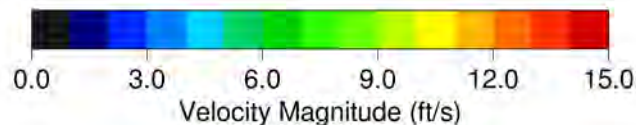


Final Design – CFD Results

Horizontal section cuts

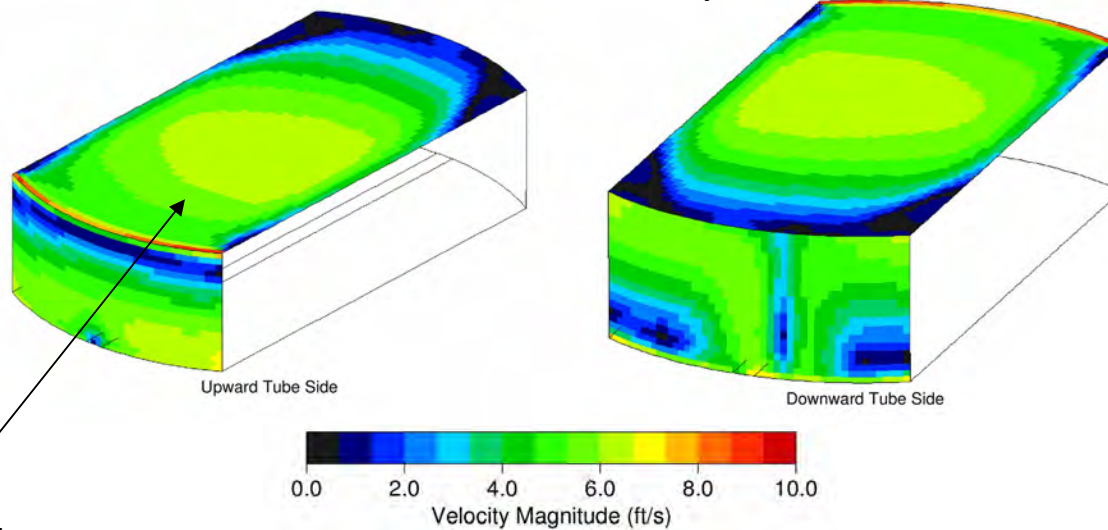


Improved uniformity between piers
Velocities still lower on average compared to top due to support structure



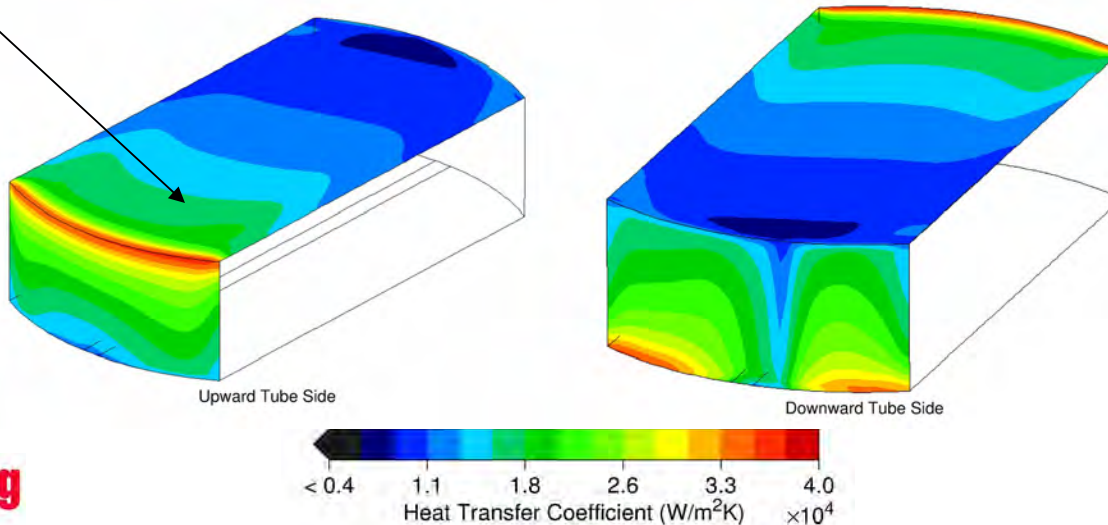
Final Design – CFD Results

Near-surface velocity

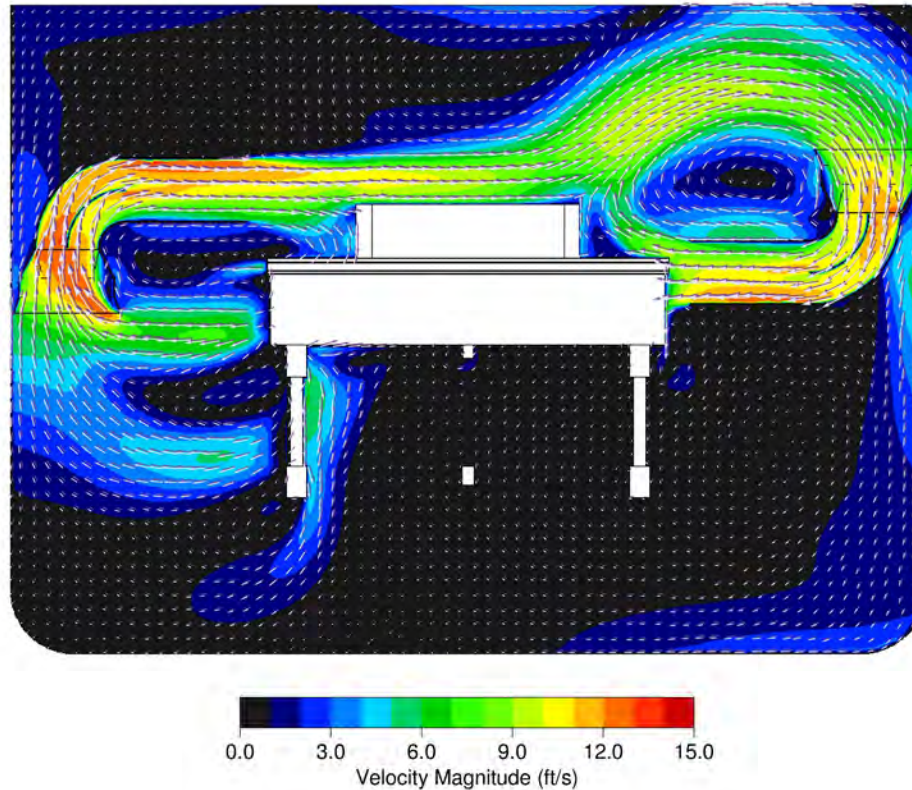


Improved side-to-side
uniformity

Surface heat transfer coefficient

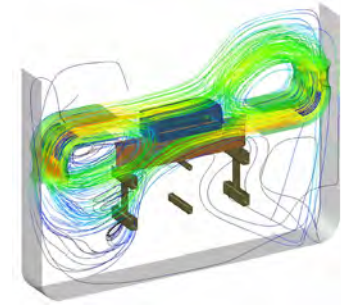
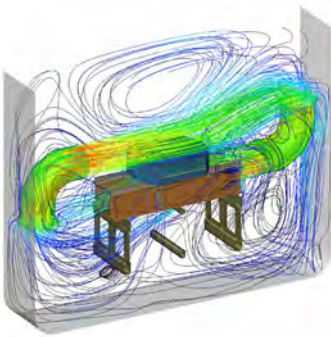


Design Validation



- Baffles in neutral position.
- 19.5 Ton load (taller than surrogate “disk” in CFD model).
- Measured velocities at outlet: 8 – 13 ft/s.
- Measured velocities near upper surface: 1.1 – 6.5 ft/s over range of elevator height.
- Measured velocities near lower surface: 0.6 – 2.2 ft/s over range of elevator height.
- All measured data per reference [2].

Conclusions



- Opposing draft tube concept creates strong circulation across width of tank.
- Spacing of the discrete tubes creates “striping” effect with low velocities between tubes.
- Flow rotation imposed by impeller creates skewed draft tube outlet profile.
- Intermediate design showed non-intuitive results with taller inlet tubes.
- Common rectangular duct with decreased impeller tube spacing improves velocity distribution between impeller tubes (along length of tank).
- Turning vane in elbow dampens flow rotation imposed by impeller.
- Variable baffle allows flow to be focused on work-zone for shorter or taller workpieces.
- Measured velocities compare favorably with predicted results.
- Detailed representation of impeller geometry could provide better prediction of actual performance curves.

References

- [1] Ansys, Fluent 6.3 User's Guide, Sect. 7.20.
- [2] Alexander, Jared C., "Trial to Determine the Suitability of the New Heat Treat Facility at Corry Forge Company for Processing Blowout Preventer Bodies", Corry Forge Company, Corry, PA, 2013.